

## Projecting peak faults and mechanical forces

### Cable cleats - Short Circuit Calculations

Below is an explanation of how CMP Products calculates Peak kA current short circuit current ratings for each specific customer application and installation.

CMP Products has carried out over 250 short circuit tests, however it is not viable to test for every fault current, cable cleat, cable size/type and fixing centre configuration!

CMP Products is continuously developing software to replicate these tests and can undertake project specific testing on the cable cleat, cable and cable tray or ladder intended to be used on the installation.

CMP also has the experience to reliably calculate what the Peak kA short circuit rating will be, based upon the expansive test data it holds following the comprehensive testing programme it has undertaken.

### Testing

Beginning with a short circuit test at 300mm fixing centres, the maximum safe Peak current in kA that the cable cleat under test can restrain is established and achieved.

In the example below the cable cleat successfully passed the tests in the IEC 61914:2009 standard at 190kA on Ø36mm cable @ 300mm fixing centres.

### Calculating the max force per cable cleat tested

From that test result the calculation from the cable cleat standard IEC 61914:2009 is used to work out the force restrained by the cable cleat under test:

$F_t$  is the maximum force on the cable (N/m)

$i_p$  is the peak short circuit current (kA)

$S$  is the centre to centre distance between two neighbouring conductors  
i.e. for trefoil formation this is the cable outside diameter (m)

In this example the  $F_t$  equals 170,472.22 N/m

$F_t$  is a force in Newtons per metre so to calculate the maximum force which each cable cleat restrained, this must be multiplied by the cable cleat fixing centres:

Max force per cable cleat =  $F_t$  (N/m) x fixing centres (m)

Max force per cable cleat in this example (0.3m fixing centres) = 51,141.67 N

### Calculating the $F_t$ for a new application

Now that the maximum force per cable cleat has been established, the formula is transposed to calculate the maximum peak fault current for different fixing centres, cable diameters etc.

To calculate the  $i_p$  if the fixing centres were to be increased 600mm then  $F_t$  would first need to be calculated:

$F_t$  is the maximum force on the cable (N/m)

$i_p$  is the peak short circuit current (kA)

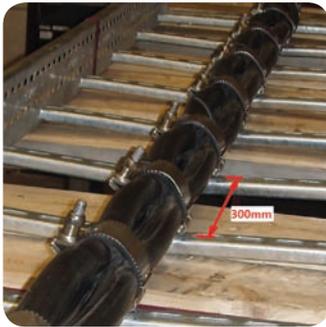
$S$  is the centre to centre distance between two neighbouring conductors  
i.e. the cable outside diameter (m)

$F_t$  in this new example = 85,236.11 (N/m)

Now that the  $F_t$  for this application has been established, the  $i_p$  can be calculated.



Before short circuit test



After short circuit test

$$F_t = \frac{0.17 \times i_p^2}{S}$$

$$F_t = \frac{0.17 \times 190^2 \text{ (kA)}}{0.036 \text{ (m)}}$$

$$F_t = \frac{\text{max force per cable cleat (N)}}{\text{fixing centres (m)}}$$

$$F_t = \frac{51,141.67 \text{ (N)}}{0.6 \text{ (m)}}$$



## Calculating the $i_p$ for a new application

$F_t$  is the maximum force on the cable (N/m)

$i_p$  is the peak short-circuit current (kA)

$S$  is the centre to centre distance between two neighbouring conductors  
i.e. the cable outside diameter (m)

$i_p$  in this example = 134.35kA

Experience shows that this value is always lower than can be achieved in a physical test. This confirms that there is a safety factor element included in the IEC 61914:2009 calculation; this is a good thing as it means that calculated values are always on the conservative side.

However it also means that the  $F_t$  or maximum force per cable cleat ratings taken from test results should only be used on fixing centre intervals which are shorter than those actually tested, as a basis for any calculated  $i_p$ 's. Calculating the opposite way is not recommended as it contradicts the safety factor employed in the standard and gives unrealistic and unachievable  $i_p$ 's.

### For example

On the same cable cleat and cable the cable cleat successfully passed the tests in the 61914:2009 standard at 150kA @ 600mm fixing centres (calculated  $i_p$  was only 134.35kA so in practice ~12% more was achieved)

From this new  $i_p$  an  $F_t$  is calculated:

$F_t$  is the maximum force on the cable (N/m)

$i_p$  is the peak short circuit current (kA)

$S$  is the centre to centre distance between two neighbouring conductors  
i.e. the cable outside diameter (m)

In this example the  $F_t$  = 106,250 N/m

Max force per cable cleat in this example (0.6m fixing centres) = 63,750 N

If this maximum force per cable cleat value was to be used as a basis to calculate the  $i_p$  for fixing centres of 0.3m, then the  $F_t$  would = 212,500 N/m

This gives a calculated  $i_p$  of 212.13kA – THIS IS DANGEROUSLY HIGH!  
Only 190kA was achieved @ 300mm fixing centres under physical test and that showed that the cable cleat was very close to its maximum strength capabilities.

### To re-confirm:

The  $F_t$  or maximum force per cable cleat ratings from test results should only be used for any calculated  $i_p$ 's when shorter fixing centre intervals than those tested are intended to be used. Calculating the opposite way is dangerous, as it contradicts the safety factor employed in the standard and gives unrealistic and unachievable  $i_p$ 's.

For the most accurate and safest installation, CMP recommends that the test result closest to the target fixing centres is used to calculate the  $i_p$ , for example:

If 600mm centres are required, the 300mm centres force per cable cleat data should be used as a basis for the  $i_p$  calculation.

If 1200mm centres are required, the 600mm centres force per cable cleat data should be used as a basis for the  $i_p$  calculation.

$$i_p = \sqrt{\left(\frac{F_t \times S}{0.17}\right)}$$

$$i_p = \sqrt{\left(\frac{85,236.11 \text{ (N/m)} \times 0.036 \text{ (m)}}{0.17}\right)}$$

$$F_t = \frac{0.17 \times i_p^2}{S}$$

$$F_t = \frac{0.17 \times 150^2 \text{ (kA)}}{0.036 \text{ (m)}}$$